

ENERGY MANAGEMENT WORKSHOP 2007

Energy Benchmarking

WHAT WE HAVE LEARNED

Al Wakelin

Sensor Environmental



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It is a Valuable Tool

- However, it must be adapted to this Industry



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Adaptations

- Clusters
 - Sour gas, Sweet Gas, Conventional Oil, Heavy Oil**
- Fuel Gas Intensity
- Critical Unit Operations



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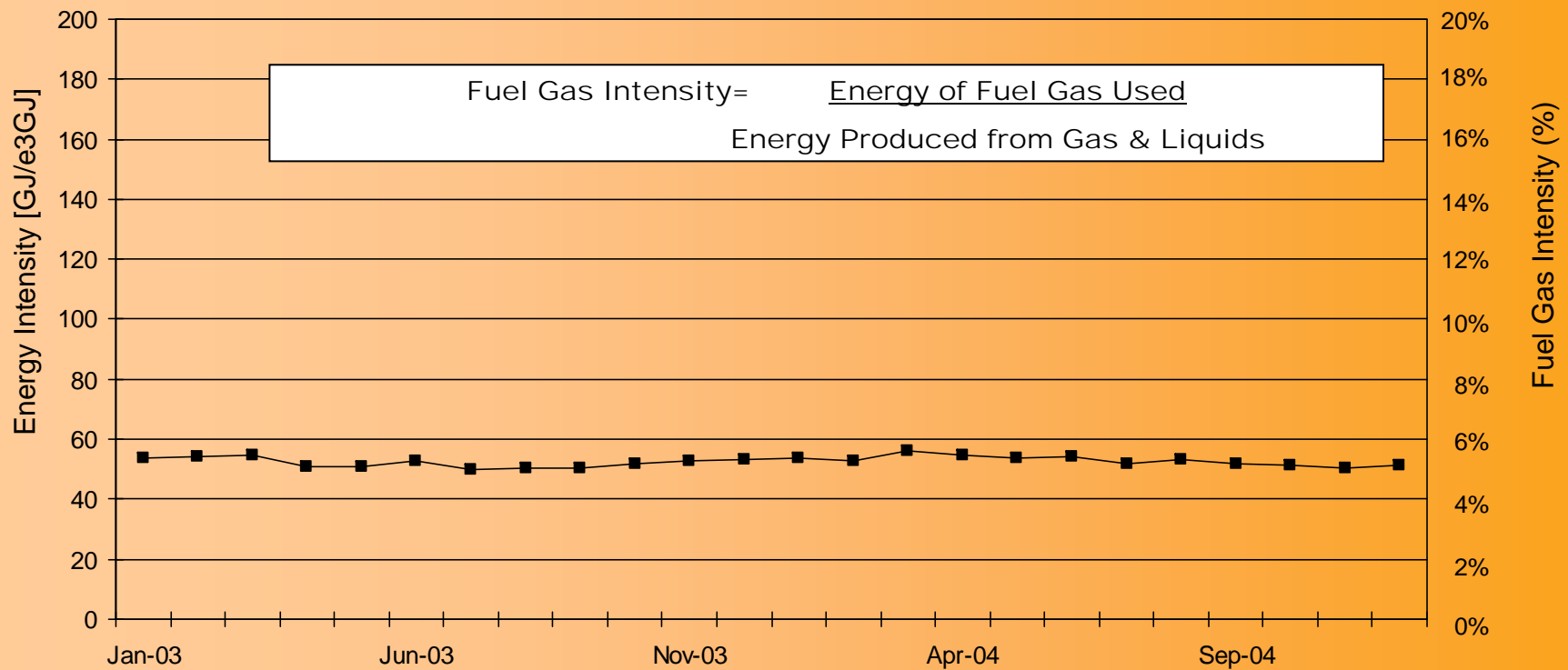


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Sweet Gas Average

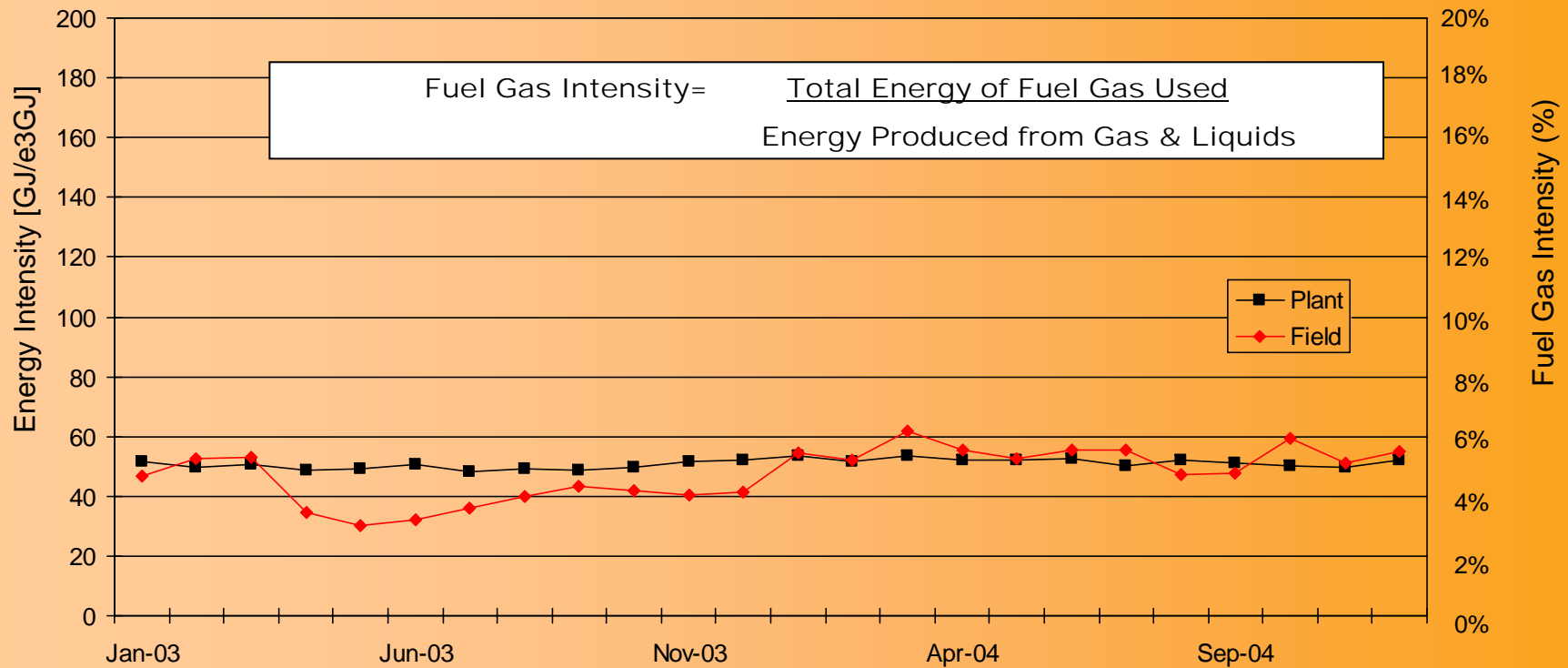


Source: EUB ST13

* every non-reported data has been excluded



Sweet Gas Plants and Field

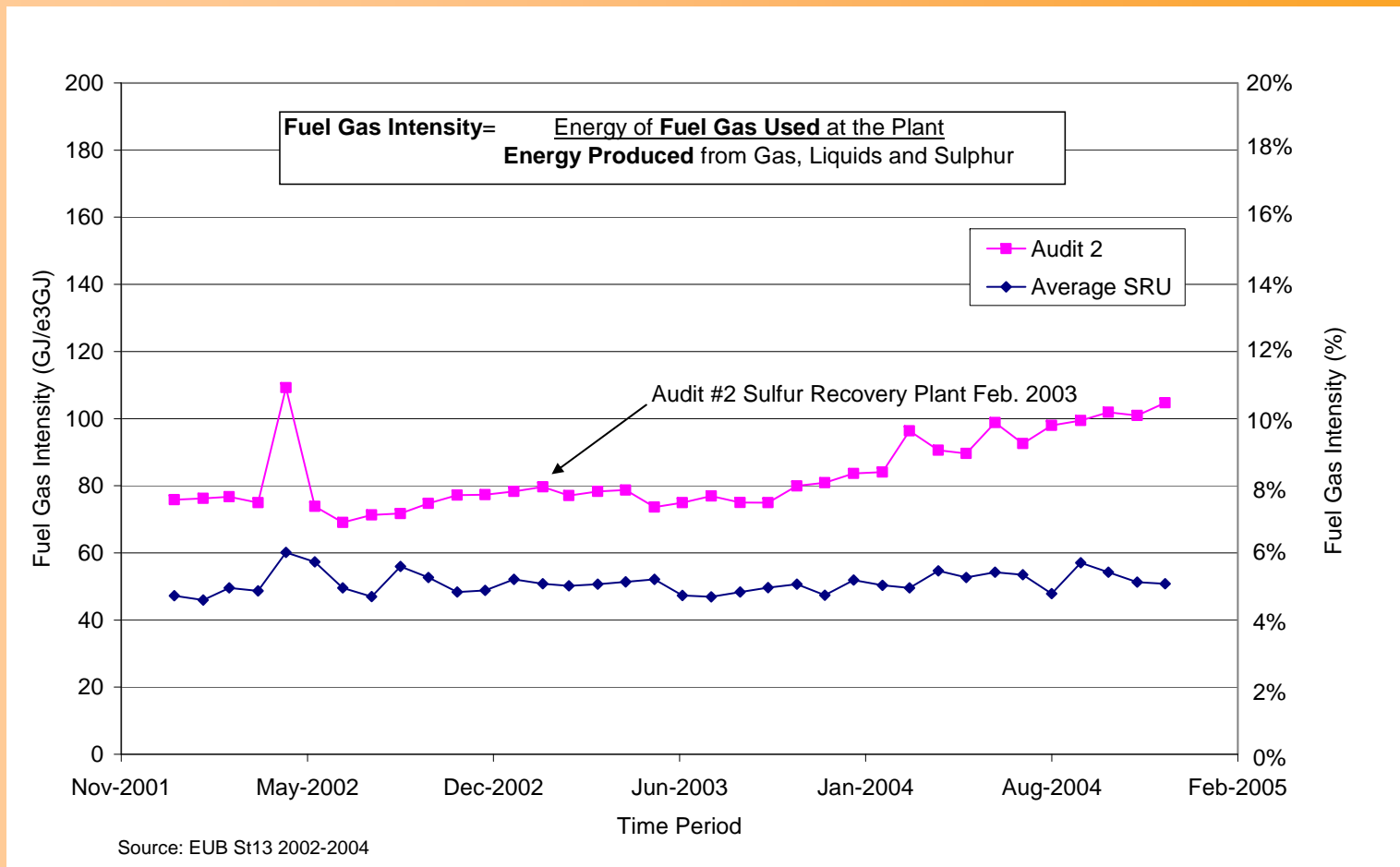


Source: EUB ST13

* every non-reported data has been excluded



Sulphur Recovery Plant



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Features

- Establish Baseline Performance
- Gauging Impact of Changes
- Compare Current Practice with Best Practices



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Optimization Tool

Amine Plant Optimization Models

Ben Spooner

Amine Experts Inc.



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Optimization Model Purpose

- Energy audits revealed root cause of high energy usage in amine plants was from over circulation (“common thread”)
 - More amine being sent to absorber than theoretically needed based on inlet H₂S and CO₂ content
- Tool developed to help determine:
 - If circulation rate can be reduced
 - If not – why not?
 - Possible engineering study
 - Cost of *not* reducing circulation rate
- **1 MW = 2.25 e³m³/day fuel gas = 4.7 t CO₂/day**



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Amine Optimization Models

□ result of GPSA calculations and simulation (ProTreat and HYSYS) results

□ circulation rate = $K(Gy/x)$

K = multiplication coefficient

G = total gas flow

y = total acid gas % (mol% H₂S + mol% CO₂)

x = amine concentration (wt %)

□ reboiler duty:

X% amine = K_x (amine circulation rate)

□ **CIRCULATION RATE DIRECTLY AFFECTS REBOILER DUTY**



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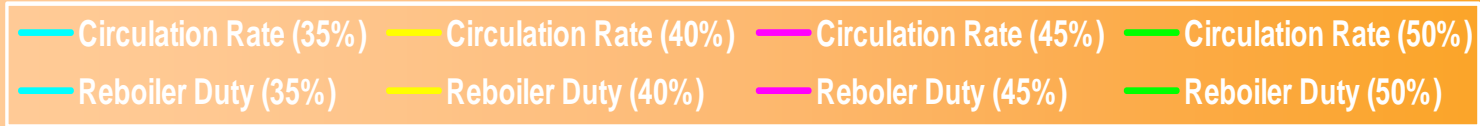
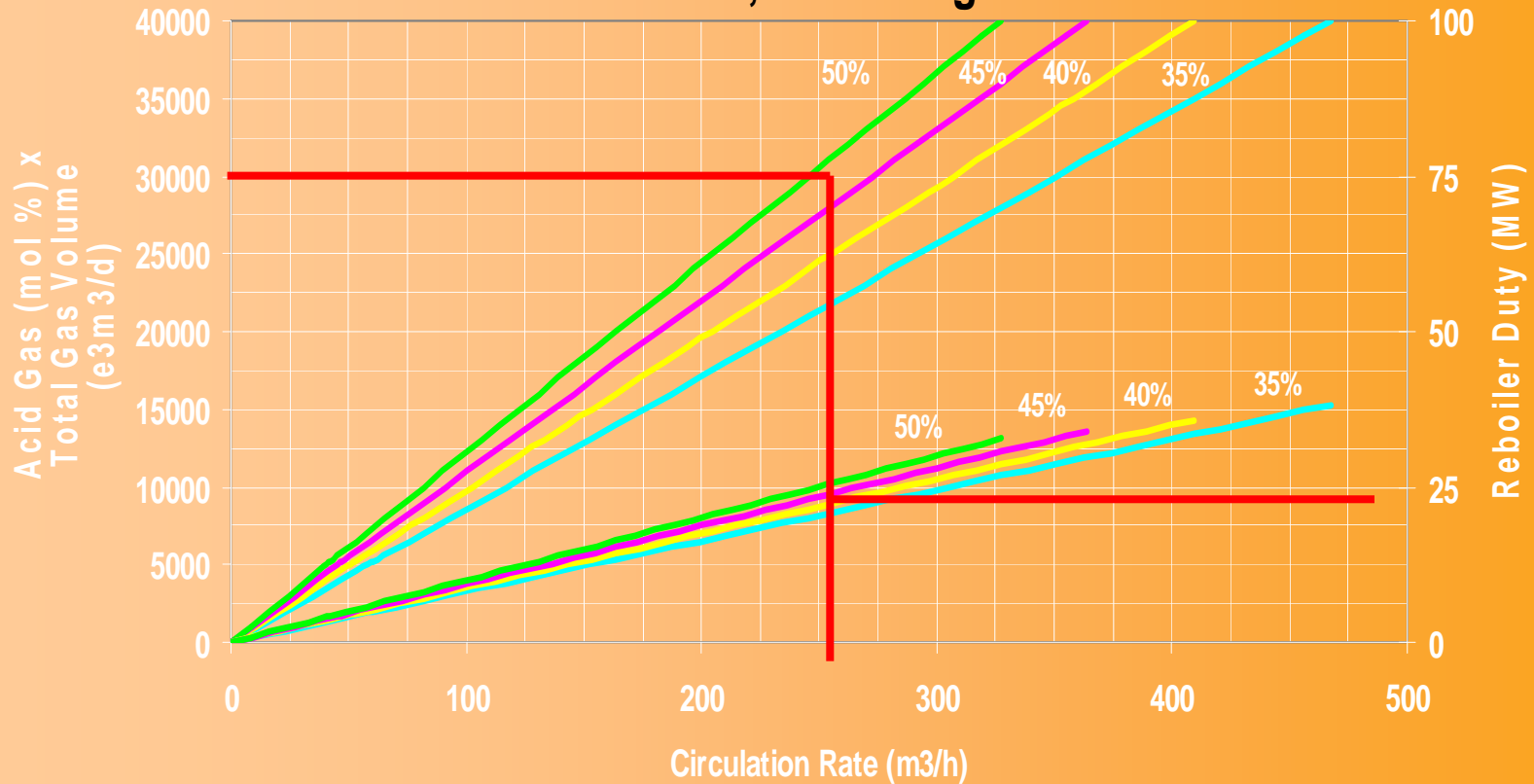


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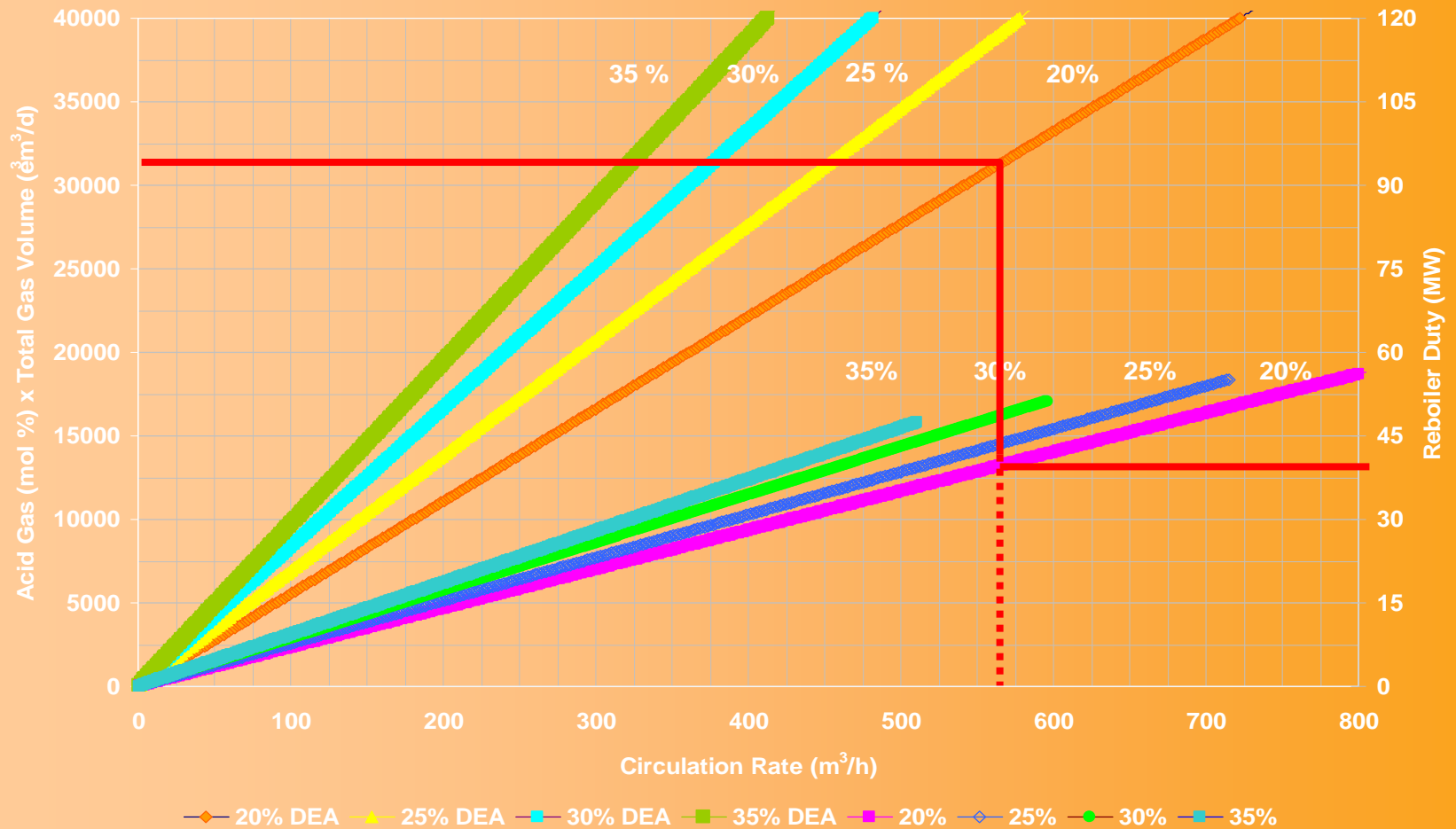
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MDEA Operating Model

3200 e³m³/d, 10% acid gas



DEA Operating Model



Model Predictions

- circulation rate will sweeten gas to below spec of 4 ppm H₂S and 2% CO₂
- corrosion mitigation
 - DEA rich loading of 0.45 – 0.55 (depending on partial pressures)
 - rich loading of 0.45 for MDEA
- reflux ratios:
 - **DEA 1.5**
 - **MDEA 1.25**
- equivalent to overhead temperature of 100°C

Assumed Parameters

- contactor sized according to inlet gas volume & pressure

- regeneration tower sized according to amine circulation rate



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Simulation Parameters

- inlet gas temperature
- inlet gas pressure: >2070 kPa / 300 psi
- lean amine temperature
- rich amine temperature (into regen tower)
- reflux temperature
- reflux pressure



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Impact of Inefficiencies

- difference between the model predictions and actual plant conditions is:
 - **impact of inefficiencies or mechanical problems in the plant**



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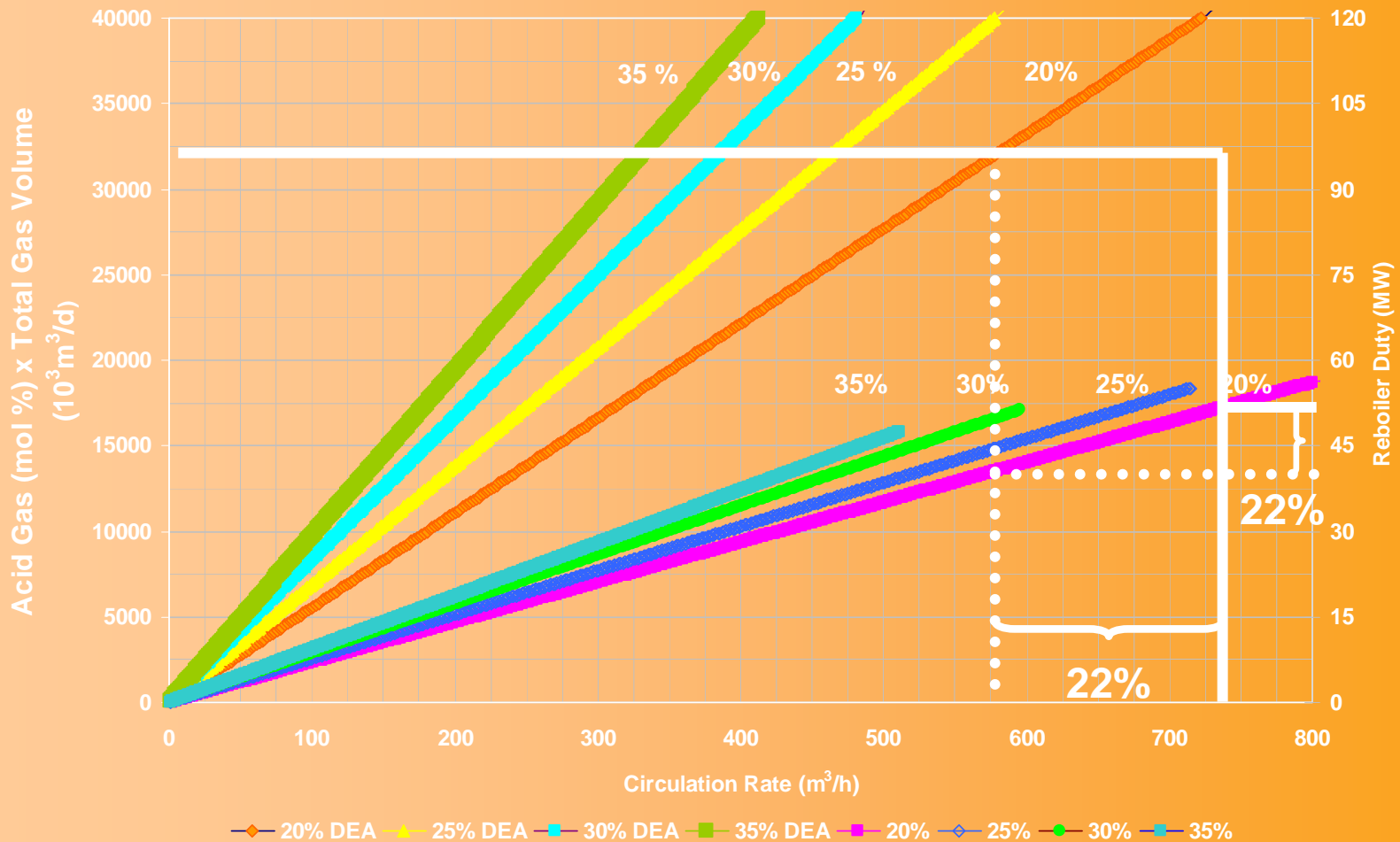
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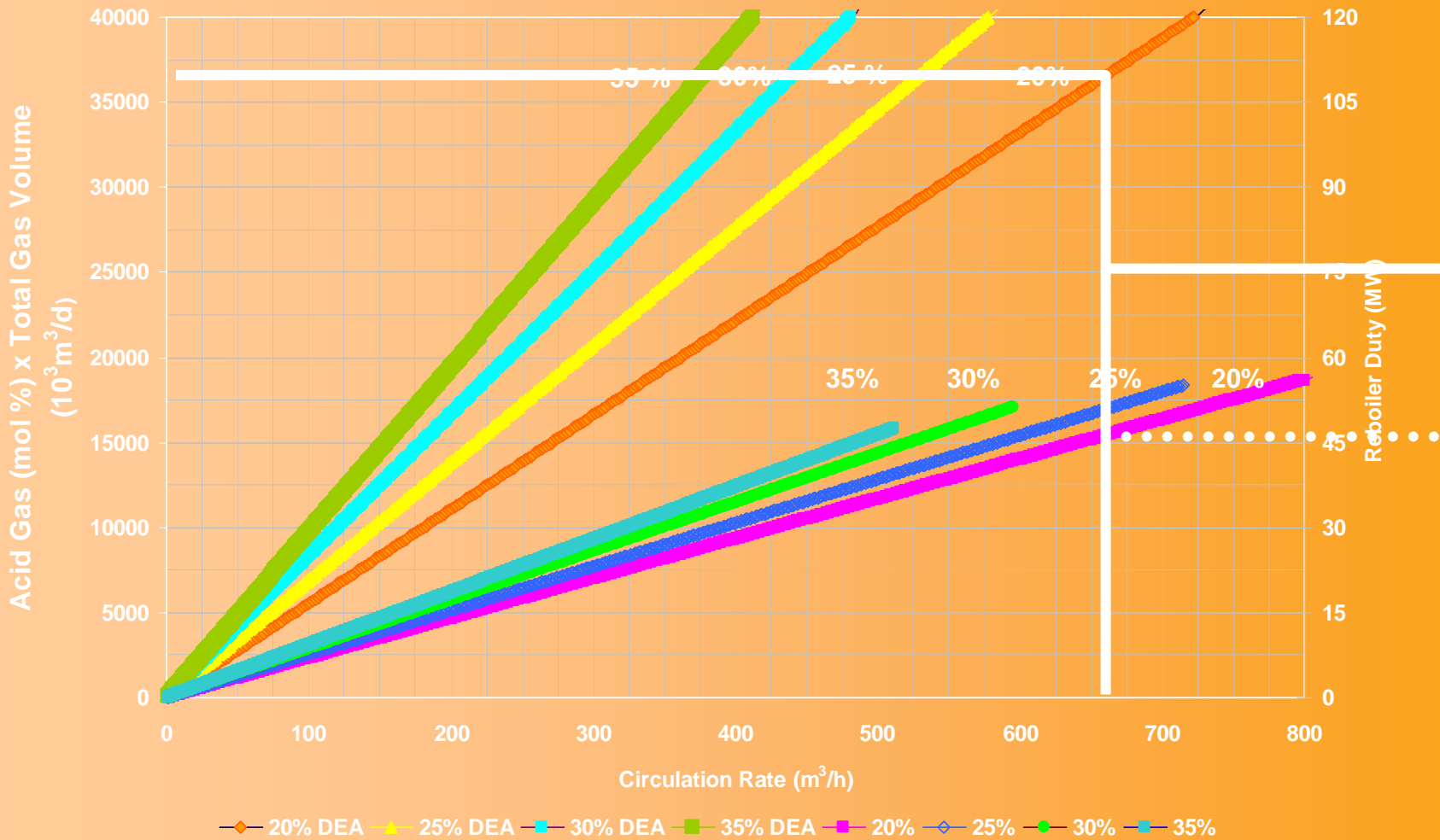
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20% DEA, 10% acid gas, 3200 $10^3\text{m}^3/\text{d}$



20% DEA, 10% acid gas, 3250 10³m³/d



Impact of Inefficiencies

- over-circulating amine can have the following negative effects...
- increased:
 - **heat duty in all aerial coolers and reboiler**
 - **pump duty**
 - **wear and tear on all equipment and piping (causing corrosion and equipment failure)**
 - **filter changes**
 - **hydrocarbon absorption**
 - **CO₂ pickup in MDEA systems**



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Model Verification

- taken onsite to various DEA & MDEA facilities
- very encouraging results
- any deviations from the graph were explainable
- generally, reboiler duty was correct for given circulation rate



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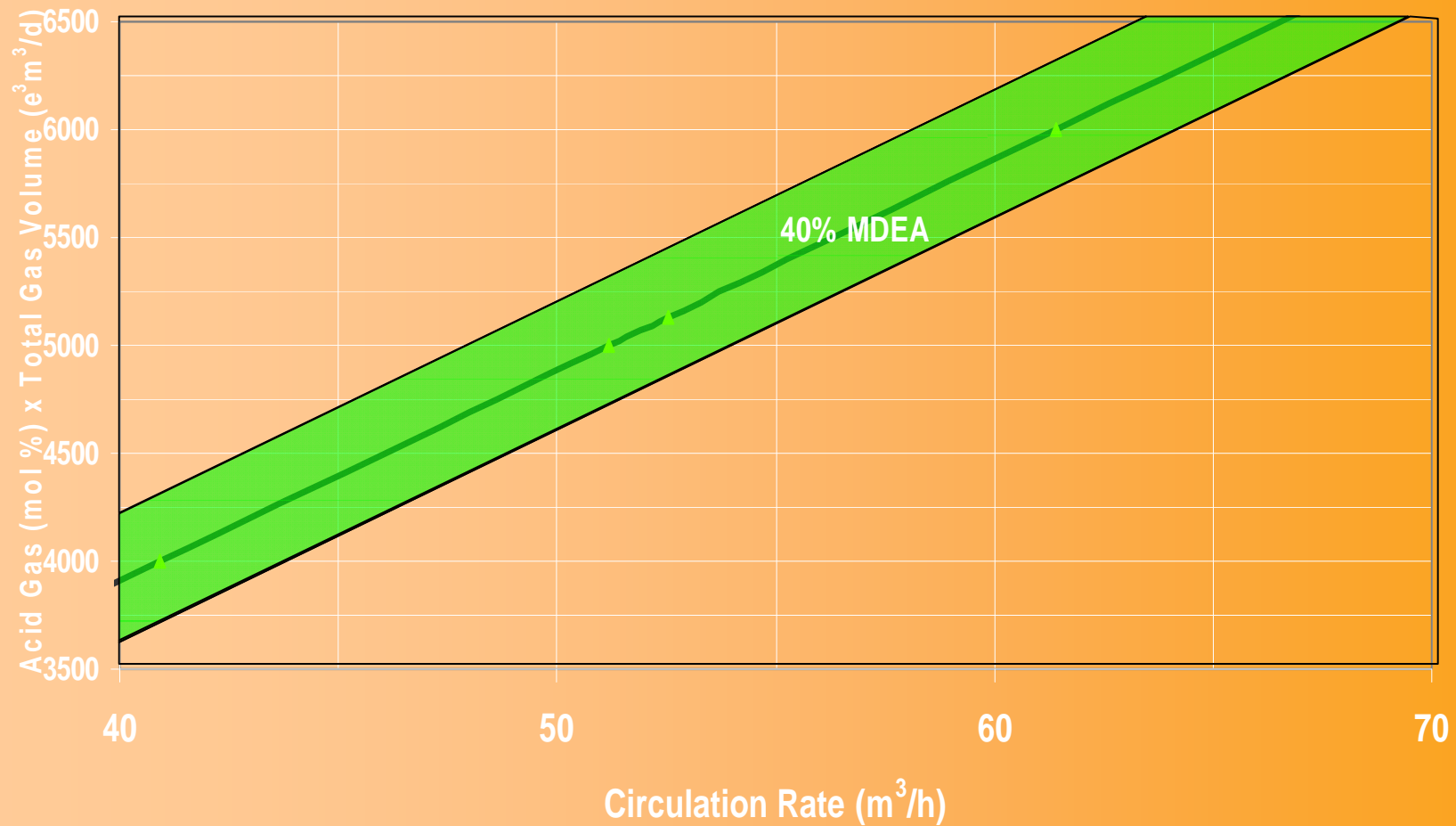
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MDEA Operating Model Circulation Rate



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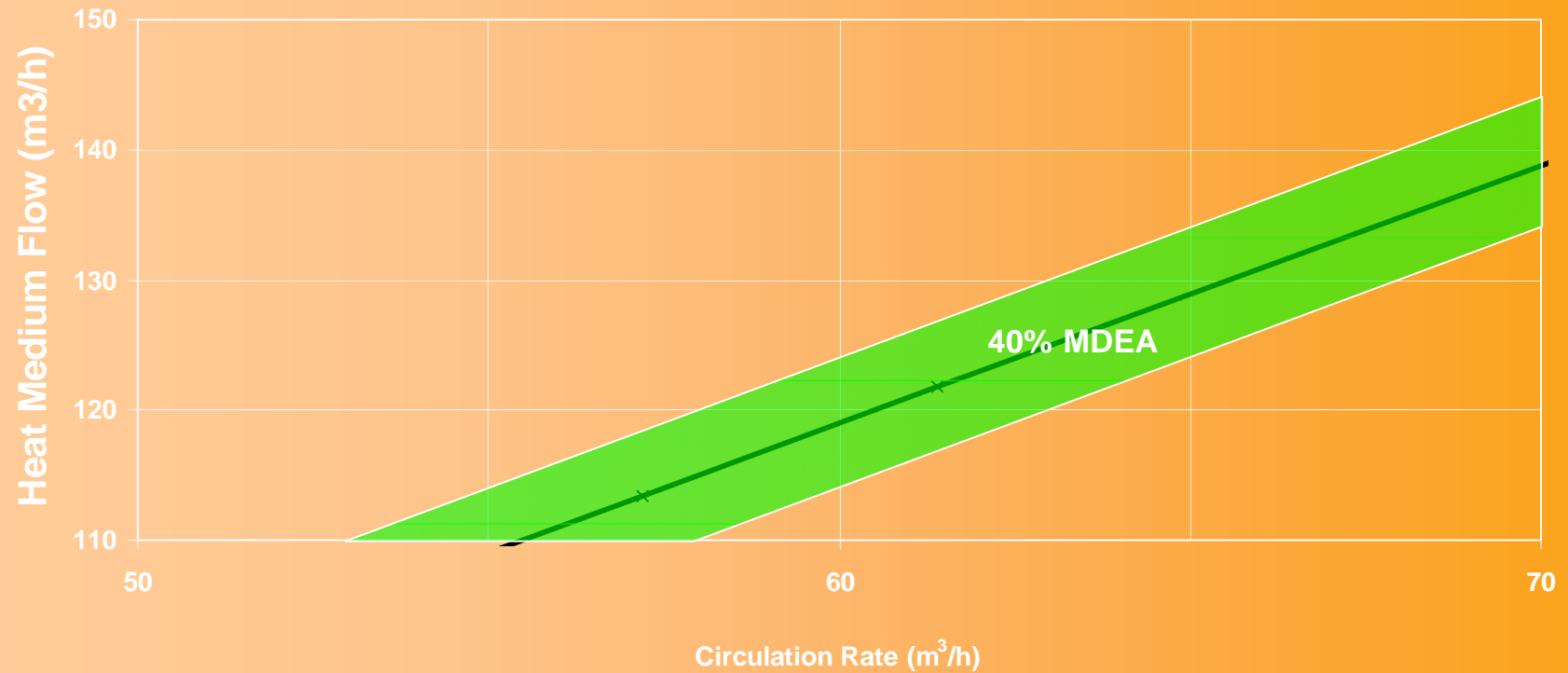
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MDEA Operating Model Reboiler Heat Medium Flow



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Next Step

- “inefficiencies”* need to be measured and trended over time
- data to be stored and displayed on DCS
- benefit of *“repairing”* inefficiency can be easily demonstrated



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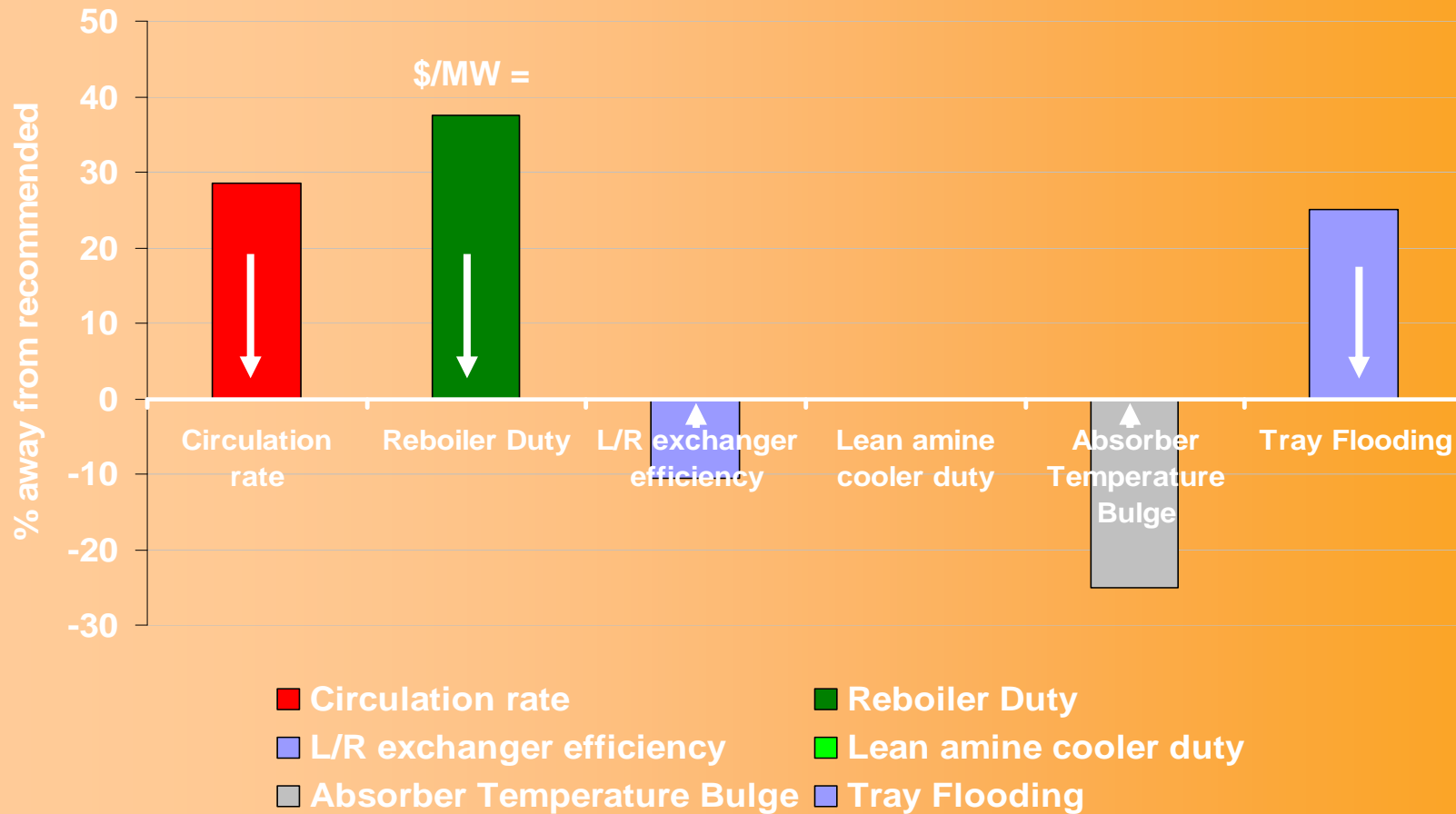
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Current Performance vs. Recommended



Summary

- makes operators life EASIER
- model prediction represents optimum operating point
- optimum KPI
- average plant over circulates by 20%:
 - **200 amine reboilers x 10 MW x 20% reduction**
= 400 MW

 - **400 MW = 900 e³m³/d fuel gas**
= \$181 912 /d (based on 38.5 GJ/e³m³)
= \$66.4 million/yr
= 1 890 t CO₂/day = 690 M t/yr



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Case Study

Glycol Dehydrator Optimization

Rod Leland
RCL Environment
Group



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Glycol Dehydrator Optimization

■ Outline

- Glycol Dehydrator Operations Overview
- Energy Consumption
- EUB Environmental Emissions Standards
 - Result in energy consumption reduction
- Operations Optimization, Emissions Reduction and Reduced Energy Consumption



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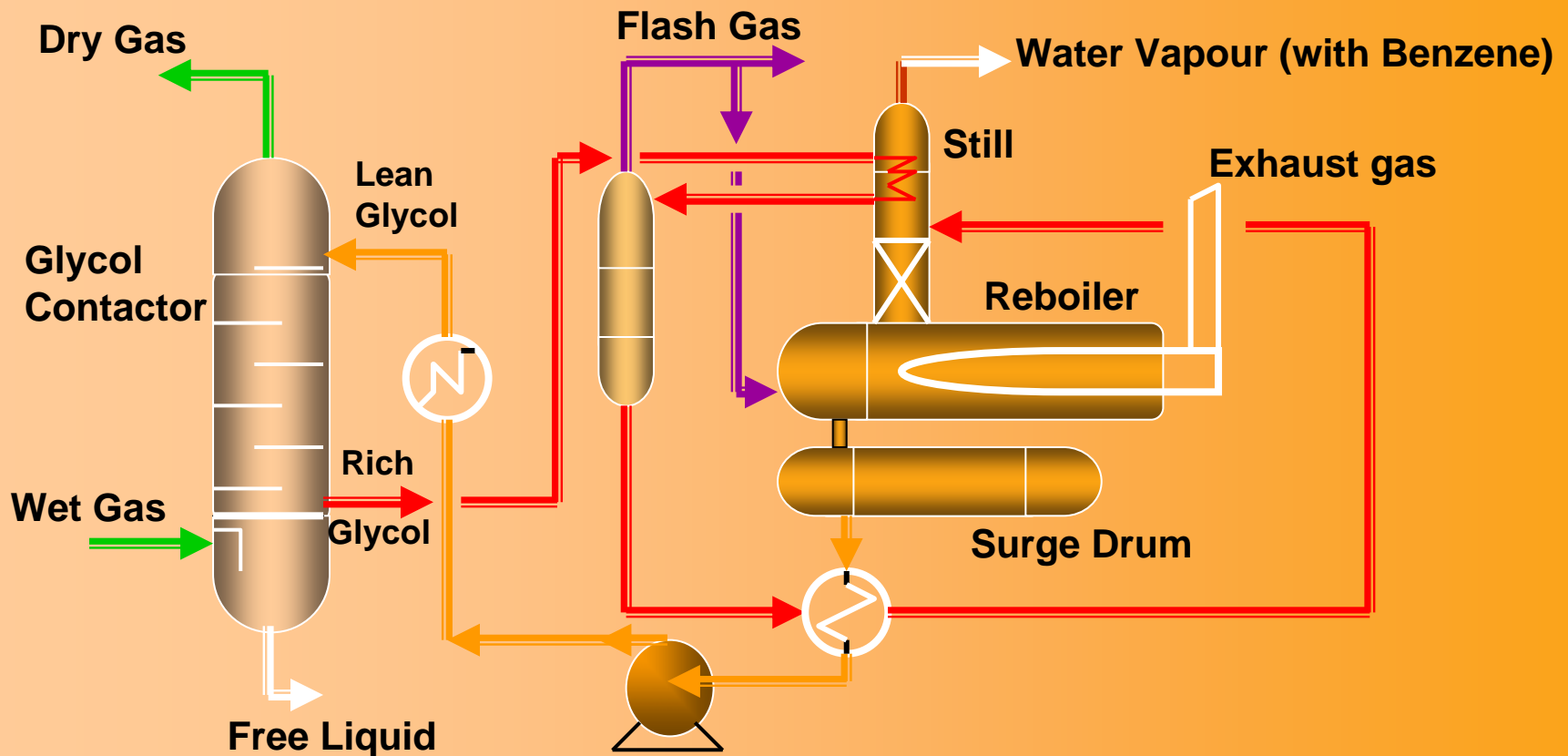
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Glycol Dehydration Schematic



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Glycol Dehydrator Optimization

■ Natural Gas Used in:

- Glycol Pumps
- Chemical Pumps
- Reboiler Burner
- Reboiler (as Stripping Gas)
- Flares and Incinerators

■ Often Used in Pumps Instead of Electricity



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Glycol Dehydrator Optimization

- Glycol circulation rate:

- Often easily changed

- Often too high

- Directly impacts:

- Benzene Emissions

- CO₂ Emissions

- Energy Consumption



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New Emission Regulations Drive Energy Conservation

- EUB Directive 39's New Requirements:
 - Lower Dehydrator Benzene Emission Limits
 - Site Emission Limits
 - Posting of Dehydrator Optimization Graph (DEOS)
 - Annual Review of Operations of Every Dehydrator



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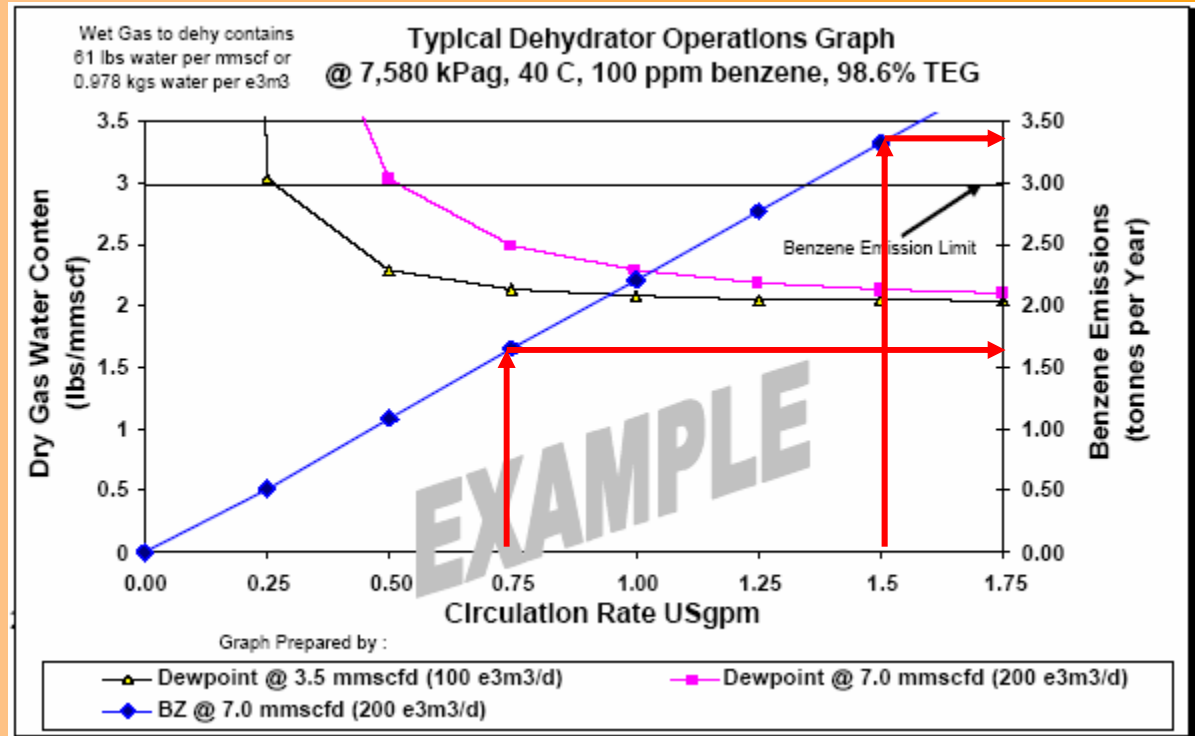


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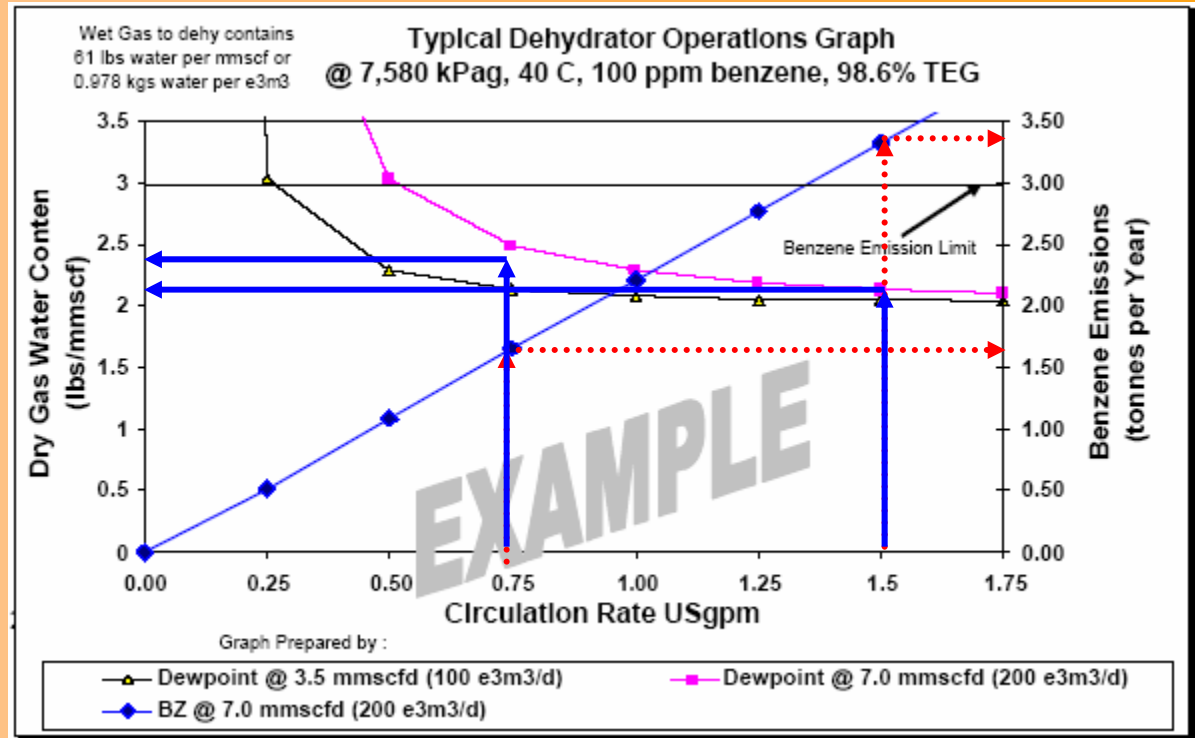
DEOS Chart

- Circulation Rate Reduction:
- Benzene Emissions are reduced by 50% by applying a 50% Circulation Rate Reduction



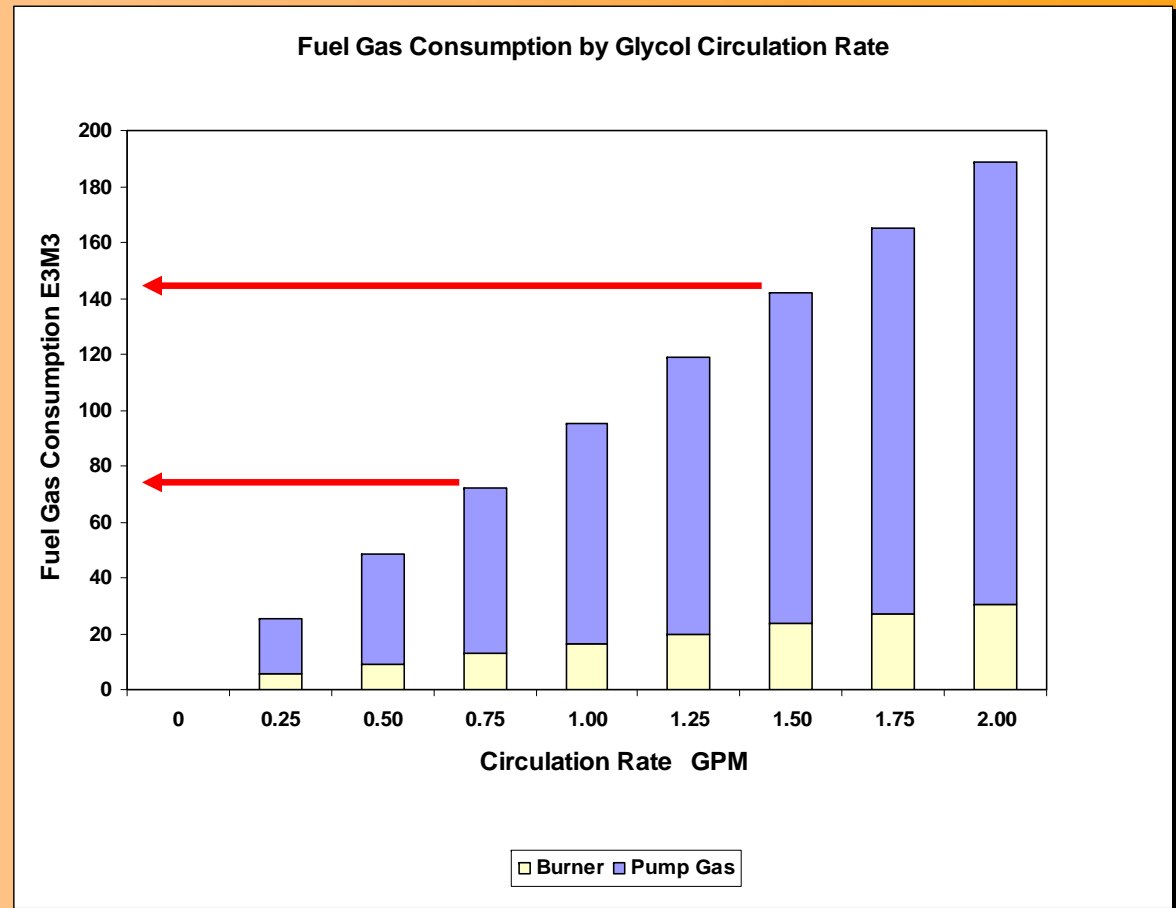
DEOS Chart

- Circulation Rate Reduction:
- Benzene Emissions are reduced by 50% by applying a 50% Circulation Rate Reduction
- Dry Gas H₂O Content Increased by 10%



Fuel Gas Reduction

- Reducing Glycol Circulation Reduces Fuel Gas Use



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Glycol Dehydrator Optimization

■ Dehydrator Statistics (2004)

- 2802 Oil and Gas Dehydrators in Alberta O&G Sector (82% of Canada's)
- Dehydrator Installation Types (~78% are all gas-driven)
 - Wellsites 44%
 - Compressors 34%
 - Gas Plants 16%
 - Batteries 6%
- Remote Sites - Significant Optimization Opportunity



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Glycol Dehydrator Optimization

■ Considerations:

- Optimization usually requires no capital expenditure
- Often Significant Energy Use Reductions
- Annual Review Required → Continuous Improvement
- Improved Environment = Improved Economy



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Methane Savings from Dehydrators and Compressors

Energy Management Workshop for Upstream and Midstream Operations

January 17, 2006

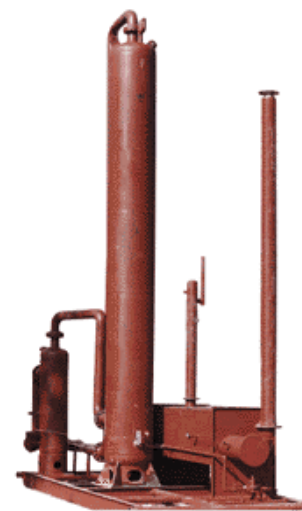


Agenda

- Dehydrators
 - Glycol Circulation Rate
 - Flash Tank Separators
- Compressors
 - Reciprocating Compressors
 - Centrifugal Compressors
- Discussion Topics
- Contact Information

Dehydrators: What is the Problem?

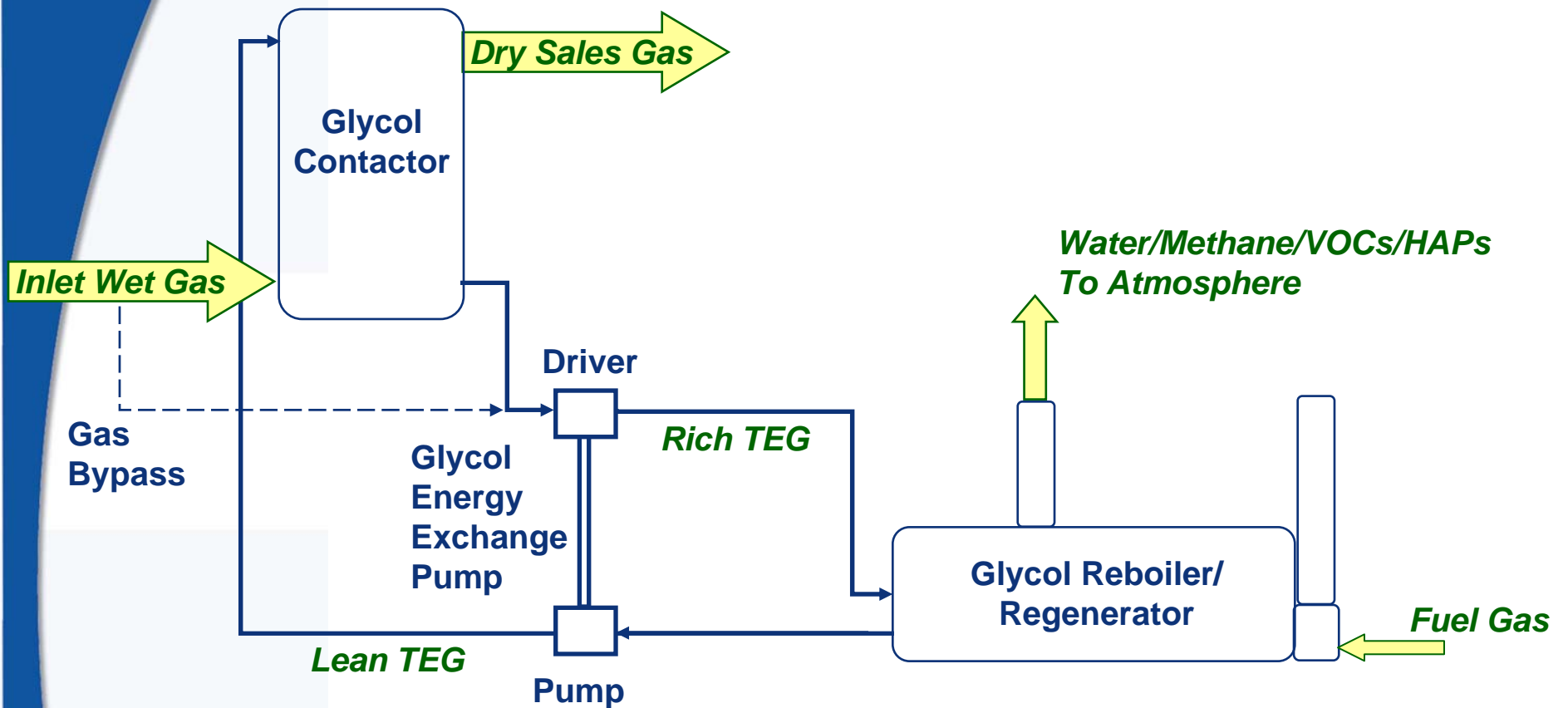
- Produced gas is saturated with water, which must be removed for gas transmission
- Glycol dehydrators are the most common equipment to remove water from gas
 - Dehydration systems in natural gas production, gathering, and boosting
 - Most use triethylene glycol (TEG)
- Glycol dehydrators create emissions
 - Methane and other hydrocarbons from reboiler vent
 - Methane from pneumatic controllers
 - On average, 275 cubic feet (cf) of methane emissions per million cf of gas processed¹



Source: www.prideofthehill.com

¹ Methane Emissions from the Natural Gas Industry, Volume 14: Glycol Dehydrators, USEPA, June 1996.

Basic Glycol Dehydrator System Process Diagram



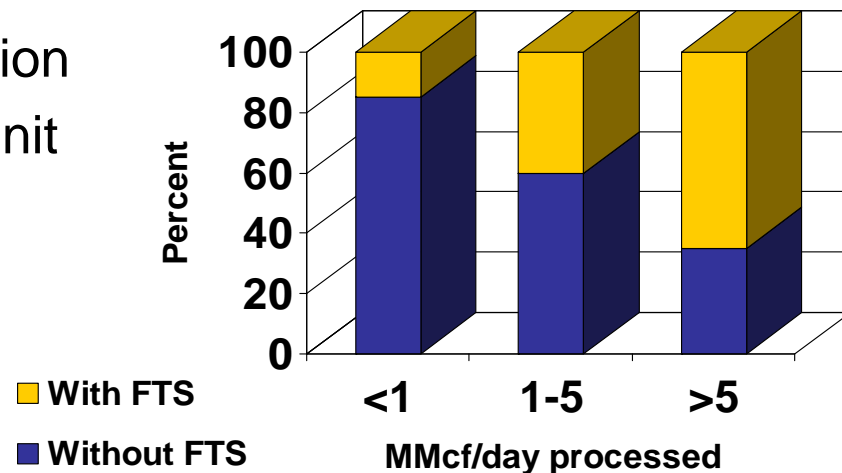
VOCs = Volatile Organic Compounds
HAPs = Hazardous Air Pollutants

Solution: Optimizing Glycol Circulation Rate

- Gas pressure and flow at gathering/booster stations vary over time
 - Glycol circulation rates are often set at a maximum circulation rate
- Glycol overcirculation results in more methane emissions without significant reduction in gas moisture content
 - Methane emissions are directly proportional to circulation
 - Operators have found circulation rates two to three times higher than necessary
- Gas STAR Lessons Learned has calculations to optimize circulation rates, save gas

Solution: Installing Flash Tank Separator (FTS)

- Flashed methane can be captured using a FTS
- Many units are not using a FTS (see bar chart)
- Recovers about 90% of methane emissions
- Reduces volatile organic compounds by 10 to 90%
- Must have an outlet for low pressure gas
 - Fuel
 - Compressor suction
 - Vapor recovery unit



MMcf = Million Cubic feet

Source: API

Economics of Flash Tanks

- Capital and installation costs:
 - Capital costs range from \$6,750 to \$13,500 per flash tank
 - Installation costs range from \$3,300 to \$5,900 per flash tank
- Negligible operational & maintenance costs

Methane Savings: Dehydrators

Two Options for Minimizing Glycol Dehydrator Emissions

Option	Capital Costs	Annual Operational & Maintenance Costs	Emissions Savings	Payback Period ¹
Optimize Circulation Rate	Negligible	Negligible	130 to 13,133 Mcf/year	Immediate
Install Flash Tank	\$6,500 to \$18,800	Negligible	236 to 7,098 Mcf/year	4 to 11 months

¹ Gas price of \$7/Mcf



Industry Experience

- One operator routes gas from FTS to fuel gas system, saving 24 Mcf/day (8,760 Mcf/year) at each dehydrator unit
- Texaco (now Chevron) installed FTS
 - Recovers 98% of methane from the glycol
 - Reduced emissions from 1,232 - 1,706 Mcf/year to less than 47 Mcf/year

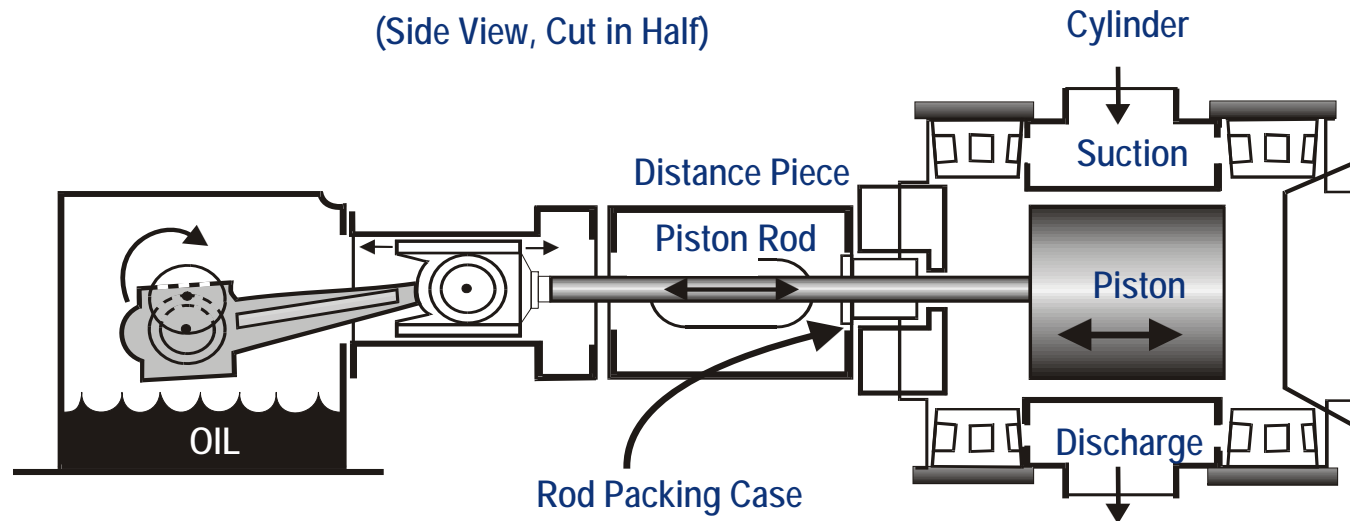


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 - Centrifugal Compressors
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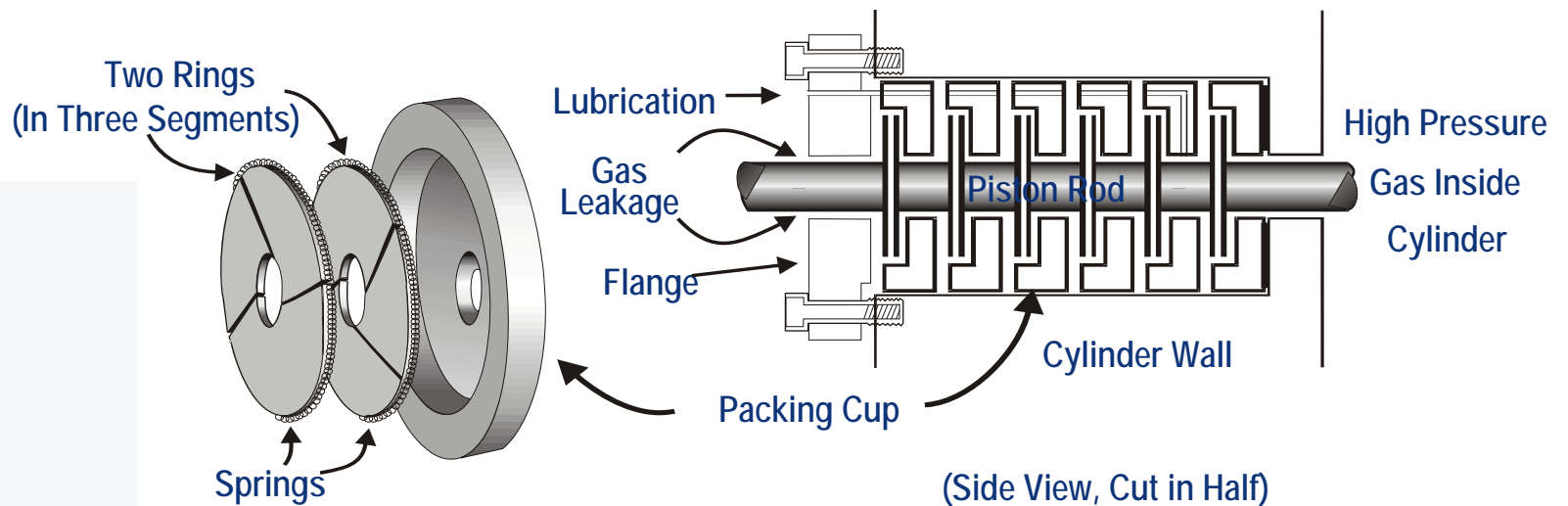
Reciprocating Compressors: What is the Problem?

- Reciprocating compressor rod packing leaks some gas by design
 - Newly installed packing may leak 60 cf/hour
 - Worn packing has been reported to leak up to 900 cf/hour



Reciprocating Compressors: What is the Problem?

- A series of flexible rings fit around the shaft to prevent leakage
- Leakage may still occur through nose gasket; between packing cups; around the rings; and between rings and shaft



Methane Savings Through Economic Rod Packing Replacement

- Assess costs of replacements
 - A set of rings: \$675 to \$1,100
(with cups and case) \$2,100 to \$3,400
 - Rods: \$2,500 to \$13,500
 - Special coatings such as ceramic, tungsten carbide, or chromium can increase rod costs
- Assess the potential savings
 - Monitor and record baseline packing leakage (usually on new packing) and piston rod wear
 - Periodically compare current leak rate to initial leak rate to determine leak reduction expected
 - Replace rod packing when the leak reduction expected is equal to or exceeds the economic replacement threshold

Solution: Rod Packing Replacement

- Economic Replacement Thresholds

Rings Only

Rings: \$1,620
 Rod: \$0
 Gas: \$7/Mcf
 Operating: 8,000 hours/year

Leak Reduction Expected (cf/hour)	Payback (years)
32	1
17	2
12	3
9	4

Rods and Rings

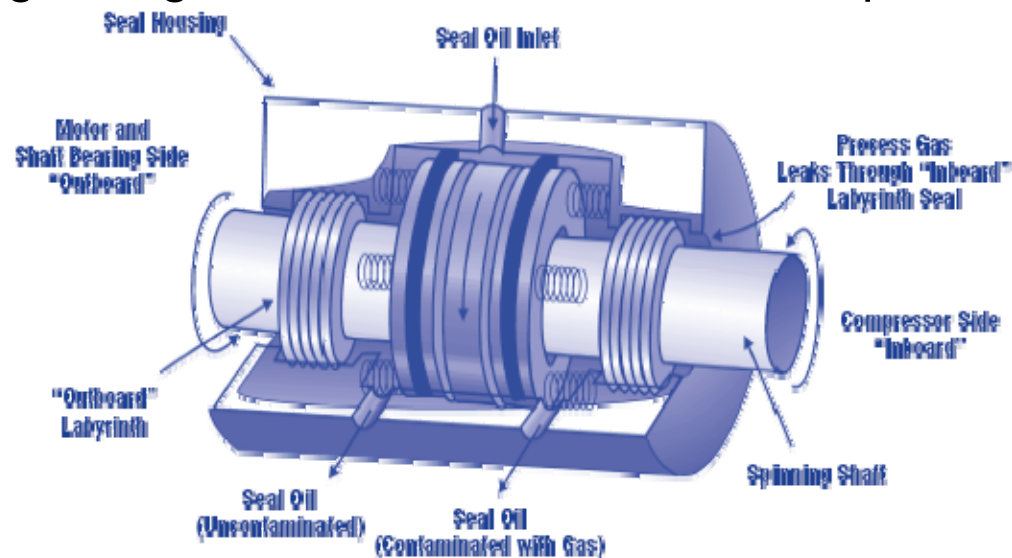
Rings: \$1,620
 Rod: \$9,450
 Gas: \$7/Mcf
 Operating: 8,000 hours/year

Leak Reduction Expected (cf/hour)	Payback (years)
217	1
114	2
79	3
62	4

Based on 10% interest rate

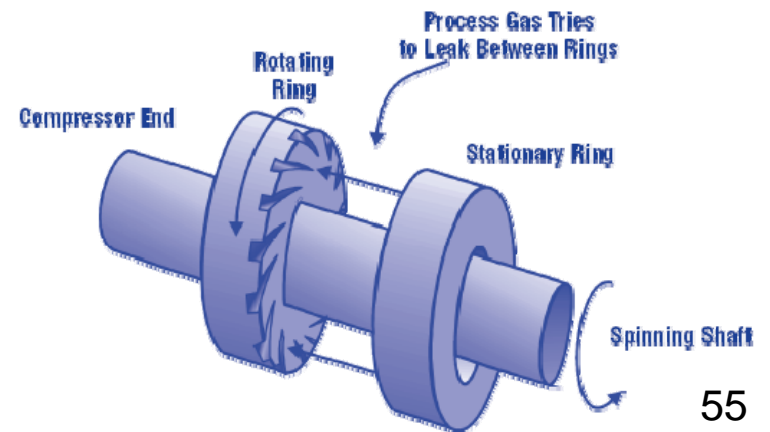
Centrifugal Compressors: What is the Problem?

- Centrifugal compressor wet seals leak little gas at the seal face
 - Seal oil degassing may vent 40 to 200 cubic feet per minute (cf/minute) to the atmosphere
- High pressure seal oil circulates between rings around the compressor shaft
- Gas absorbs in the oil on the inboard side
- Little gas leaks through the oil seal
- Seal oil degassing vents methane to the atmosphere



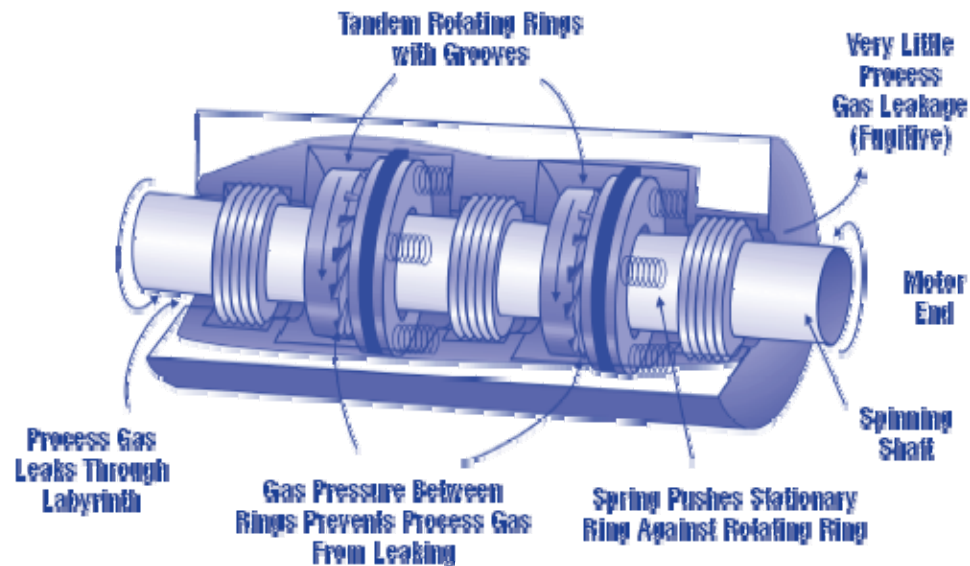
Solution: Replace Wet Seals with Dry Seals

- Dry seal springs press the stationary ring in the seal housing against the rotating ring when the compressor is not rotating
- At high rotation speed, gas is pumped between the seal rings by grooves, creating a high pressure barrier to leakage
- Only a very small amount of gas escapes through the gap



Methane Savings: Dry Seals

- Dry seals typically leak at a rate of only 0.5 to 3 cf/minute
 - Significantly less than the 40 to 200 cf/minute emissions from wet seals
- Gas savings translate to approximately \$112,000 to \$651,000 at \$7/Mcf



Economics of Replacing Seals

- Compare costs and savings for a 6-inch shaft beam compressor

Cost Category	Dry Seal (\$)	Wet Seal (\$)
Implementation Costs¹		
Seal costs (2 dry @ \$13,500/shaft-inch, w/testing)	\$162,000	
Seal costs (2 wet @ \$6,7500/shaft-inch)		\$81,000
Other costs (engineering, equipment installation)	\$162,000	\$0
Total Implementation Costs	\$324,000	\$81,000
Annual O&M	\$14,100	\$102,400
Annual Methane Emissions (@ \$7/Mcf; 8,000 hours/year)		
2 dry seals at a total of 6 cf/minute	\$20,160	
2 wet seals at a total of 100 cf/minute		\$336,000
Total Costs Over 5-Year Period	\$495,300	\$2,273,000
Total Dry Seal Savings Over 5 Years		
Savings	\$1,777,700	
Methane Emissions Reductions (Mcf; at 45,120 Mcf/year)	225,600	

¹ Flowserve Corporation updated with Nelson Farrar indices

Discussion Topics

- Industry experience applying these technologies and practices
- Limitations on application of these technologies and practices
- Actual costs and benefits

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Optimization Tool

Monitoring & Targeting Energy Usage

Brian Tyers

Stantec Consulting



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Monitoring and Targeting

**What you do not measure,
you cannot control !!**

Tom Peters

- Monitoring and Targeting (M&T) is the backbone of any energy management program
- Energy savings, if not monitored, will quickly erode



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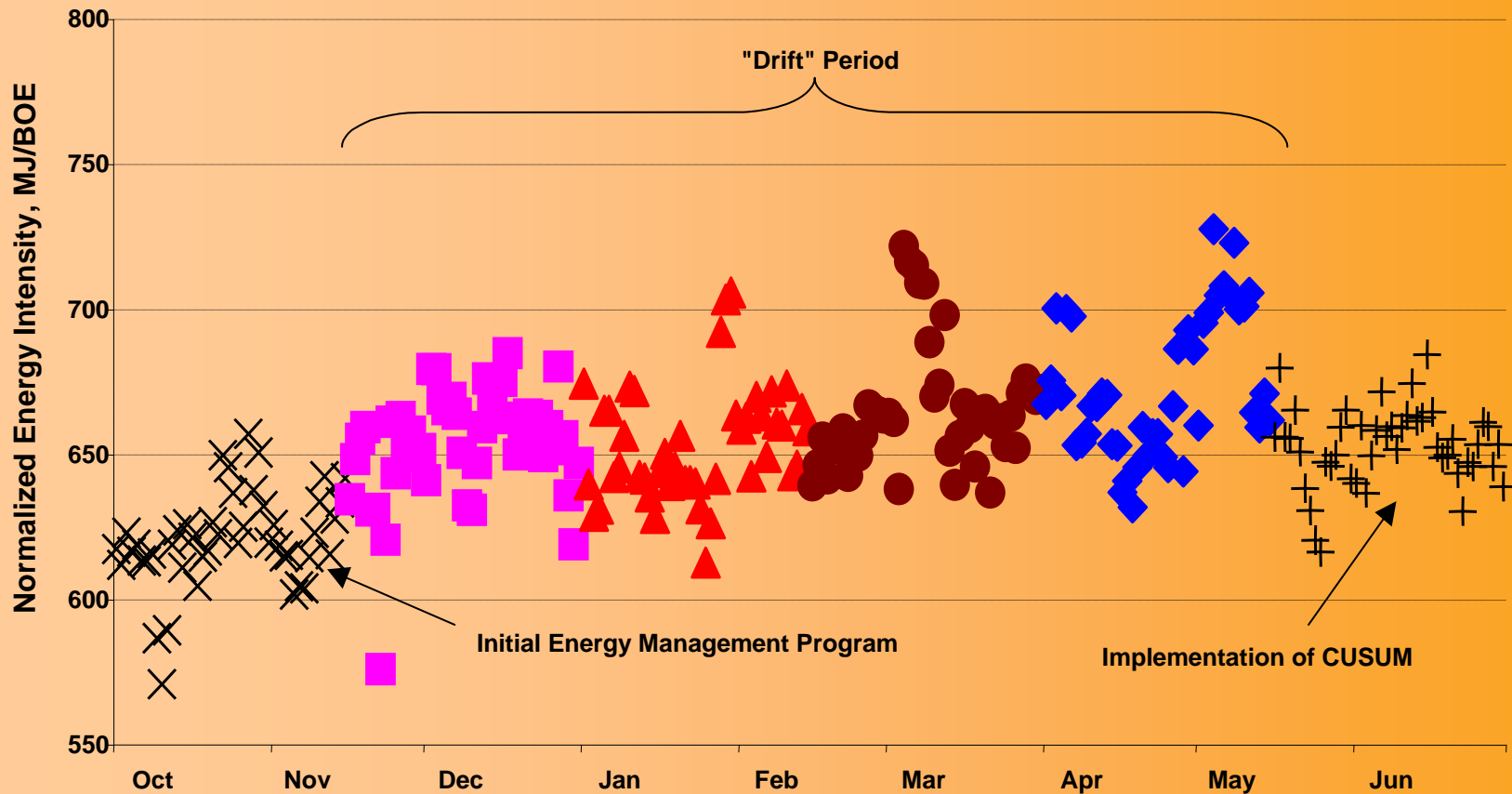
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Energy Use & Intensity “Can Drift”



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Steps

- Data collection

- Production; fuel, electrical energy

- Baseline selection

- Stable energy use pattern
- Used for gauging on-going performance



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Steps

- Estimate of difference in energy use
 - Actual energy use versus
 - Predicted energy use

- Cumulative summation of differences (CUSUM)



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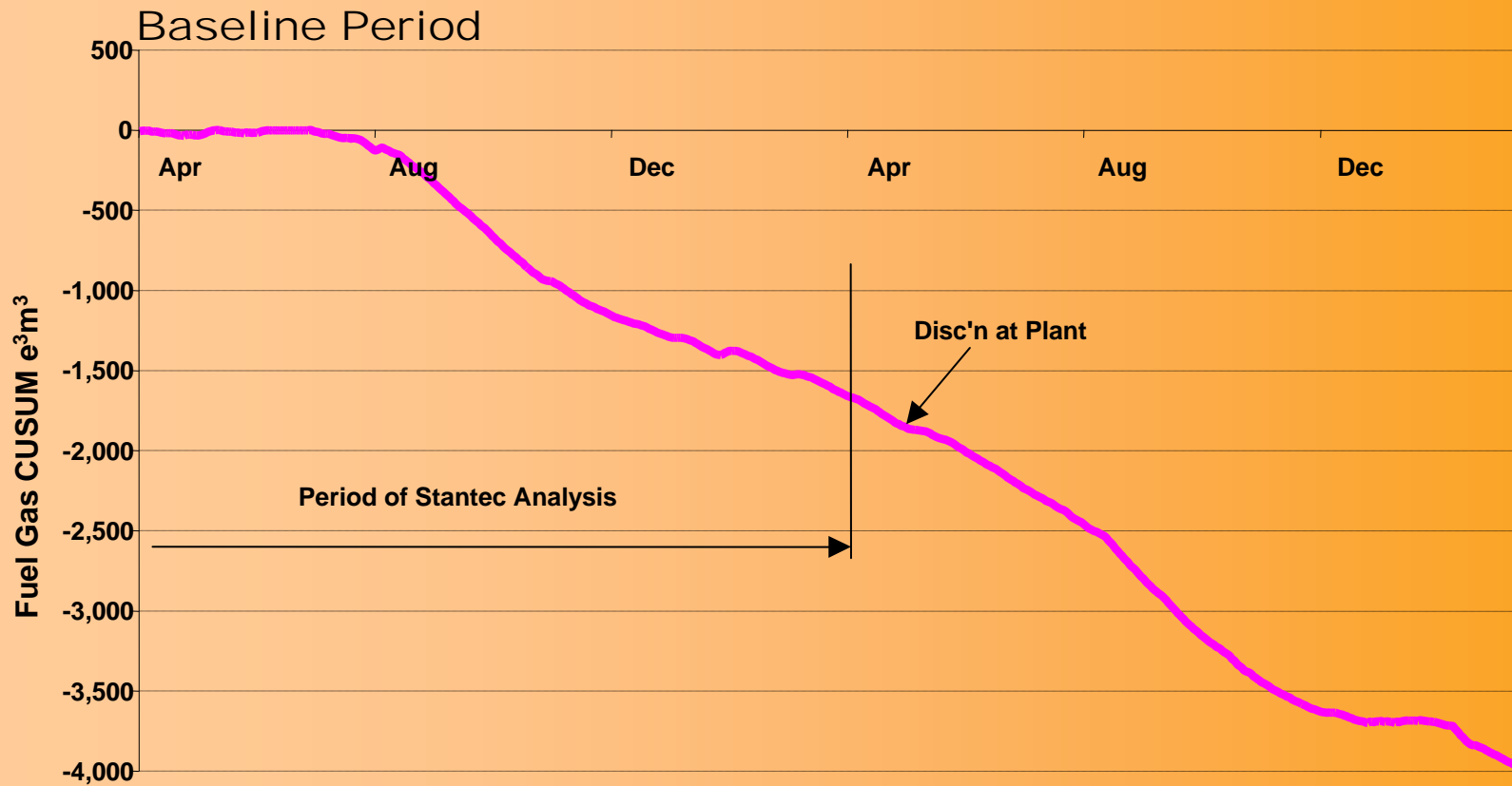
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Fuel Gas – 2003-2005



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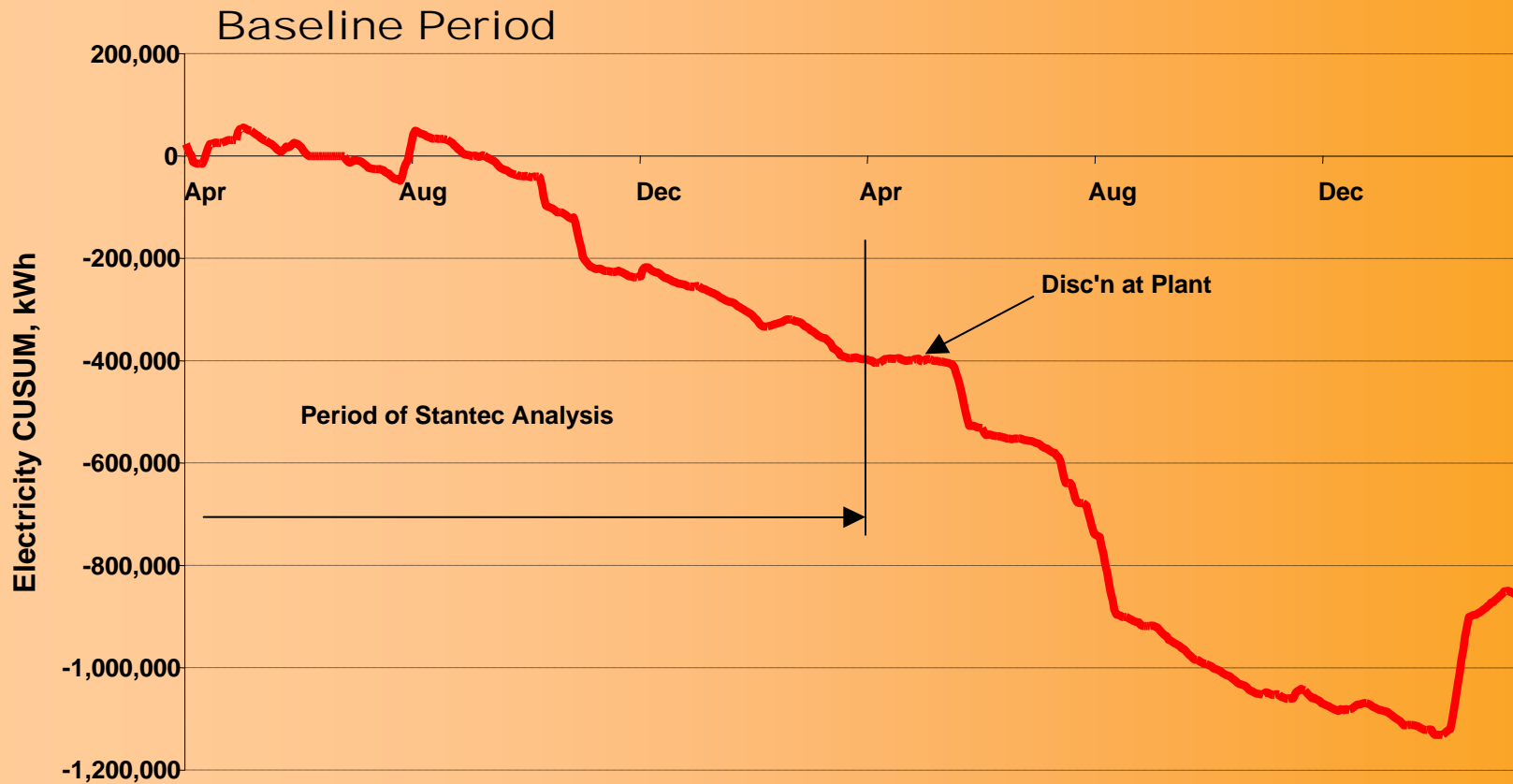
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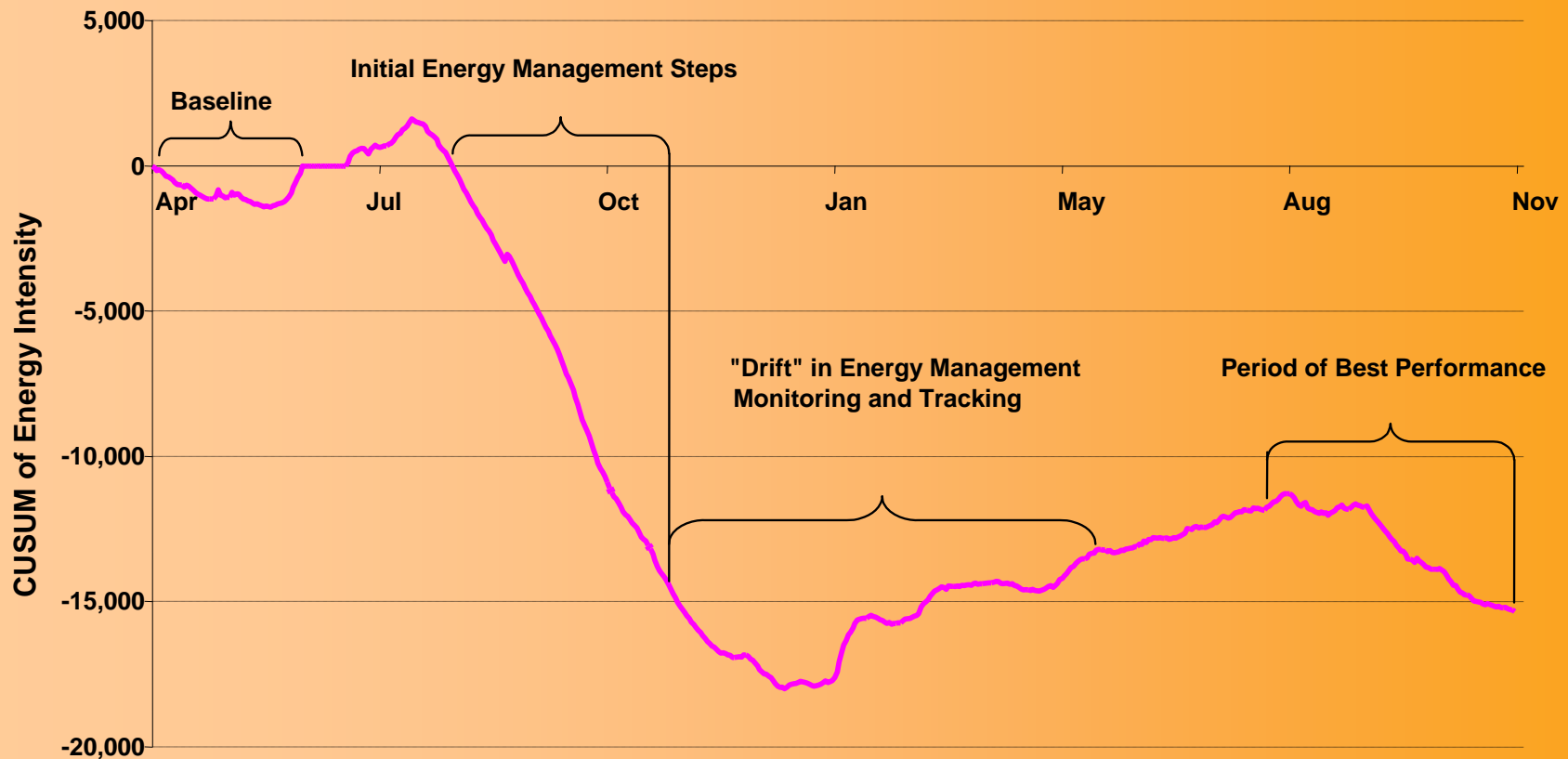
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Electrical – 2003-2005



Tracking a Key Performance Indicator (Energy Intensity)



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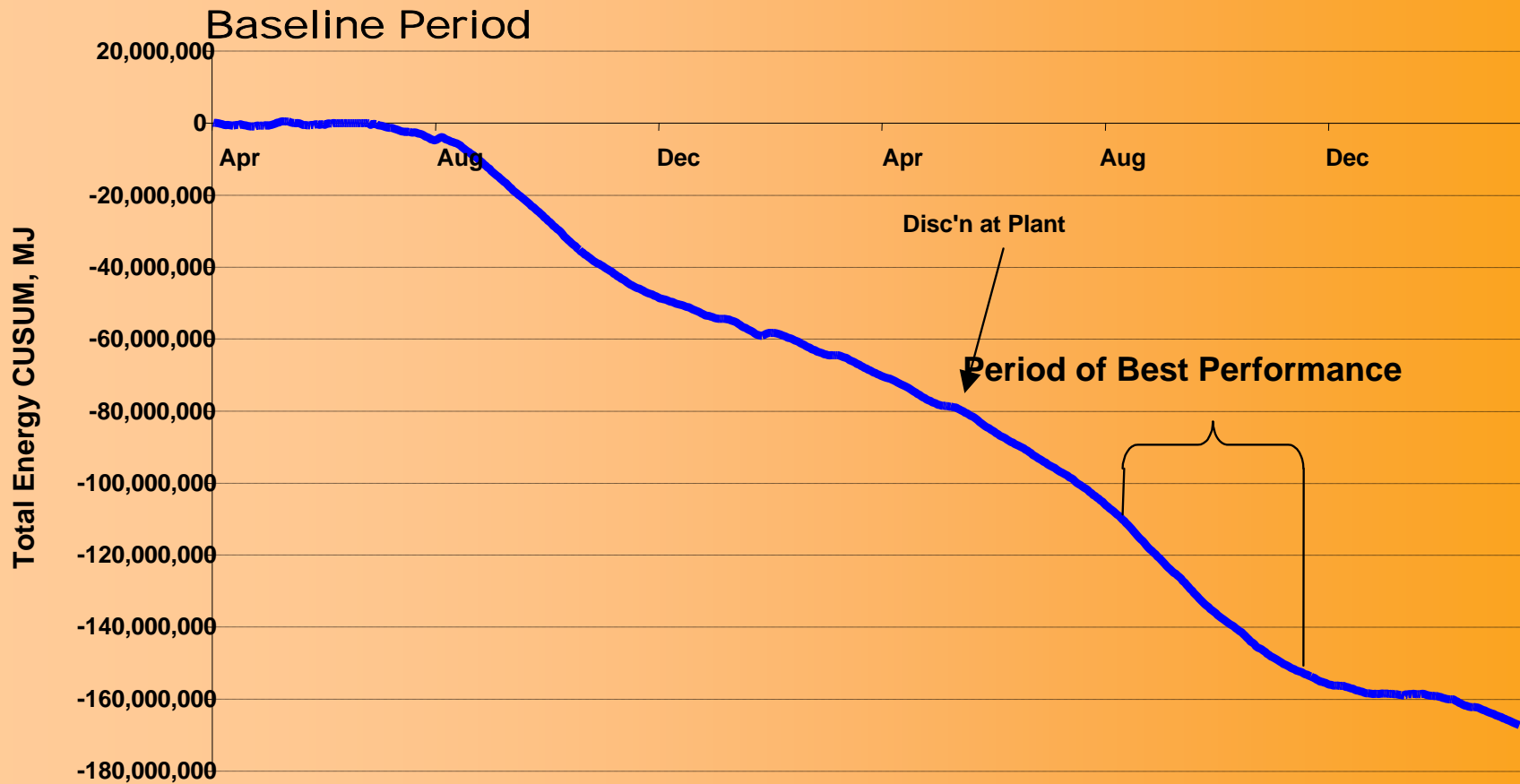


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Total Energy – 2003-2005



Conclusions

- Identify the magnitude of energy use/wastage and associated emissions and their value at the Facility level
- Establish energy/emissions baselines and intensity indices
- Motivate Staff to manage energy usage, costs and emissions
- Budget More Accurately



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